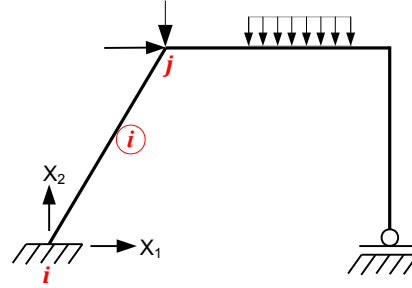




9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

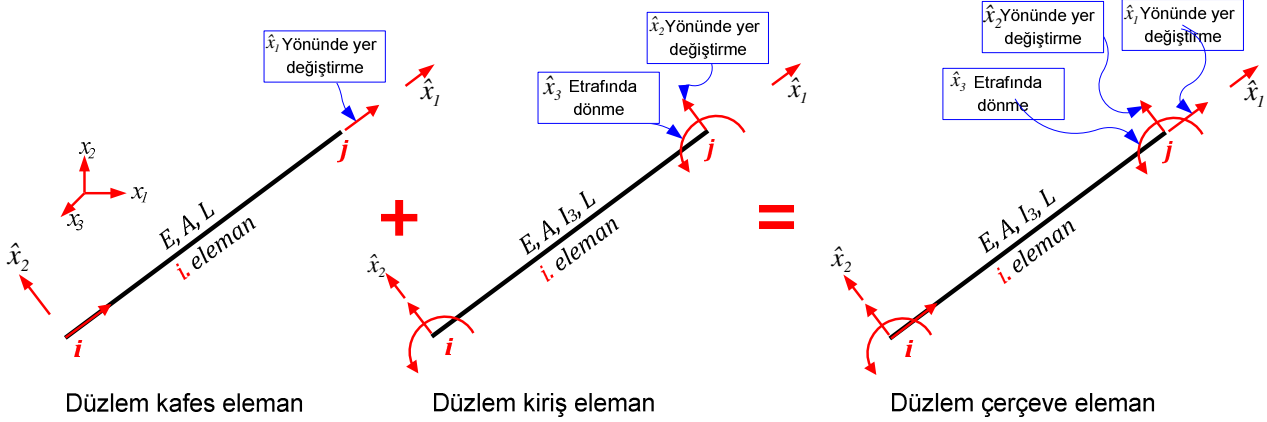
Sağdaki, x_1 - x_2 düzleminde olan çerçevenin çözümünde kullanılacak i . elemanın rijitlik ve transformasyon matrisi belirlenecektir. Yükle çerçeve düzleminde, burulma yoktur. Çerçevenin herhangi bir noktasında serbestlik derecesi=3 tür: Bir düşey+bir yatay yer değiştirme+ x_3 etrafında dönme.



Şekil 9.1 Düzlem çerçeve

9.1 Yerel rijitlik matrisi

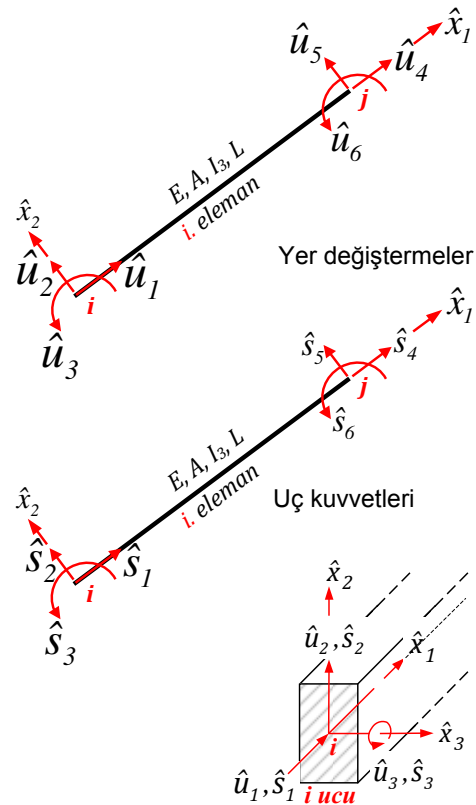
Normal kuvvet sadece elemanın eksen boyunca yer değiştirmeye (uzama-kısalma) neden olur, kesme ve momenti etkilemez. Bu nedenle çerçeve elemanı kafes eleman ile kiriş elemanın toplamı olarak düşünebiliriz:



Çerçeve elemanın yerel koordinatlardaki yer değiştirmeleri ve kuvvetleri şekil 9.2 de gösterilmiştir. \hat{x}_3 lokal eksen kâğıt(ekran) düzlemine dik ve okuyucuya doğru yönelmiştir. Yerel yer değiştirme ve kuvvet vektörleri:

$$\hat{u}^i = \begin{matrix} \hat{u}_1 \\ \hat{u}_2 \\ \hat{u}_3 \\ \hat{u}_4 \\ \hat{u}_5 \\ \hat{u}_6 \end{matrix} \begin{matrix} i \text{ noktasında } \hat{x}_1 \text{ yönünde yer değiştirme} \\ i \text{ noktasında } \hat{x}_2 \text{ yönünde yer değiştirme} \\ j \text{ noktasında } \hat{x}_3 \text{ etrafında dönme} \\ j \text{ noktasında } \hat{x}_1 \text{ yönünde yer değiştirme} \\ j \text{ noktasında } \hat{x}_2 \text{ yönünde yer değiştirme} \\ j \text{ noktasında } \hat{x}_3 \text{ etrafında dönme} \end{matrix}$$

$$\hat{s}^i = \begin{matrix} \hat{s}_1 \\ \hat{s}_2 \\ \hat{s}_3 \\ \hat{s}_4 \\ \hat{s}_5 \\ \hat{s}_6 \end{matrix} \begin{matrix} i \text{ noktasında } \hat{x}_1 \text{ yönünde aksenal kuvvet} \\ i \text{ noktasında } \hat{x}_2 \text{ yönünde kesme kuvveti} \\ i \text{ noktasında } \hat{x}_3 \text{ etrafında moment} \\ j \text{ noktasında } \hat{x}_1 \text{ yönünde aksenal kuvvet} \\ j \text{ noktasında } \hat{x}_2 \text{ yönünde kesme kuvveti} \\ j \text{ noktasında } \hat{x}_3 \text{ etrafında moment} \end{matrix}$$



Şekil 9.2: Düzlem çerçeve eleman

9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

5.12 deki kafes elemanın 2'2 boyutlu rijitlik matrisini ve 8.14 deki giriş elemanın rijitlik matrisini 6'6 boyutluya dönüştürelim

Bak: 5.12

$$\hat{k}_{kafes}^i = \frac{EA}{L} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \rightarrow \hat{k}_{kafes}^i = \begin{bmatrix} \frac{EA}{L} & 0 & 0 & -\frac{EA}{L} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ -\frac{EA}{L} & 0 & 0 & \frac{EA}{L} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

Bak: 8.14

$$\hat{k}_{kiriş}^i = \begin{bmatrix} \frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} & -\frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} \\ \frac{6EI_3}{L^2} & \frac{4EI_3}{L} & -\frac{6EI_3}{L^2} & \frac{2EI_3}{L} \\ \frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} & -\frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} \\ -\frac{6EI_3}{L^2} & -\frac{4EI_3}{L} & \frac{6EI_3}{L^2} & -\frac{2EI_3}{L} \\ \frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} & -\frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} \\ \frac{6EI_3}{L^2} & \frac{4EI_3}{L} & -\frac{6EI_3}{L^2} & \frac{2EI_3}{L} \end{bmatrix} \rightarrow \hat{k}_{kiriş}^i = \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & \frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} & 0 & -\frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{4EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{2EI_3}{L} \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -\frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} & 0 & \frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{2EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{4EI_3}{L} \end{bmatrix}$$

Düzlem çerçeve elemanın 6'6 boyutlu rijitlik matrisi $\hat{k}_{çerçeve}^i = \hat{k}_{kafes}^i + \hat{k}_{kiriş}^i$ dir:

$$\hat{k}_{çerçeve}^i = \begin{bmatrix} \frac{EA}{L} & 0 & 0 & -\frac{EA}{L} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ -\frac{EA}{L} & 0 & 0 & \frac{EA}{L} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} + \begin{bmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & \frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} & 0 & -\frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{4EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{2EI_3}{L} \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & -\frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} & 0 & \frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{2EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{4EI_3}{L} \end{bmatrix} = \begin{bmatrix} \frac{EA}{L} & 0 & 0 & -\frac{EA}{L} & 0 & 0 \\ 0 & \frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} & 0 & -\frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{4EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{2EI_3}{L} \\ -\frac{EA}{L} & 0 & 0 & \frac{EA}{L} & 0 & 0 \\ 0 & -\frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} & 0 & \frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{2EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{4EI_3}{L} \end{bmatrix}$$

$$\hat{k}^i = \begin{bmatrix} \frac{EA}{L} & 0 & 0 & -\frac{EA}{L} & 0 & 0 \\ 0 & \frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} & 0 & -\frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{4EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{2EI_3}{L} \\ -\frac{EA}{L} & 0 & 0 & \frac{EA}{L} & 0 & 0 \\ 0 & -\frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} & 0 & \frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{2EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{4EI_3}{L} \end{bmatrix} \quad \leftarrow \text{Çerçeve elemanın yerel rijitlik matrisi} \quad (9.1)$$

9.2 Düzlem çerçeve elemanın yerel denge koşulu

8.18 bağıntısı geçerlidir. Sadece matrislerin boyut ve içeriği farklıdır. \underline{s}^i eleman üzerindeki yüklerin eşdeğeri (ankastrelik kuvvetleri) olmak üzere:

$$\hat{k}^i \hat{u}^i + \underline{s}^i = \hat{s}^i \quad (9.2)$$

$$\begin{bmatrix} \frac{EA}{L} & 0 & 0 & -\frac{EA}{L} & 0 & 0 \\ 0 & \frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} & 0 & -\frac{12EI_3}{L^3} & \frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{4EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{2EI_3}{L} \\ -\frac{EA}{L} & 0 & 0 & \frac{EA}{L} & 0 & 0 \\ 0 & -\frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} & 0 & \frac{12EI_3}{L^3} & -\frac{6EI_3}{L^2} \\ 0 & \frac{6EI_3}{L^2} & \frac{2EI_3}{L} & 0 & -\frac{6EI_3}{L^2} & \frac{4EI_3}{L} \end{bmatrix} \begin{bmatrix} \hat{u}_1 \\ \hat{u}_2 \\ \hat{u}_3 \\ \hat{u}_4 \\ \hat{u}_5 \\ \hat{u}_6 \end{bmatrix} + \begin{bmatrix} \hat{s}_1 \\ \hat{s}_2 \\ \hat{s}_3 \\ \hat{s}_4 \\ \hat{s}_5 \\ \hat{s}_6 \end{bmatrix} = \begin{bmatrix} \hat{s}_1 \\ \hat{s}_2 \\ \hat{s}_3 \\ \hat{s}_4 \\ \hat{s}_5 \\ \hat{s}_6 \end{bmatrix} \quad (9.3)$$

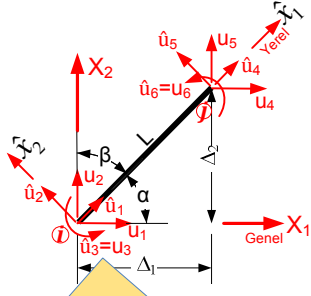
Eleman üzerindeki yüklerin eşdeğer yükleri

Eleman yerel kuvvetleri

Eleman yerel rijitlik matrisi

Eleman yerel yer değiştirmeleri

9.2 Düzlem çerçeve elemanın transformasyon matrisi



Dönme ve moment, eksenlerin dönmelerinden etkilenmez. Çünkü x_3 ve \hat{x}_3 eksenleri daima birbirine paraleldir.

x_{1i}, x_{2i} : i noktasının genel koordinatları
 x_{1j}, x_{2j} : j noktasının genel koordinatları

$$\Delta_1 = x_{1j} - x_{1i}, \quad \Delta_2 = x_{2j} - x_{2i}, \quad L = \sqrt{\Delta_1^2 + \Delta_2^2}, \quad \cos \alpha = \frac{\Delta_1}{L}, \quad \cos \beta = \frac{\Delta_2}{L}$$

$$\left. \begin{aligned} \hat{u}_1 &= u_1 \frac{\Delta_1}{L} + u_2 \frac{\Delta_2}{L} \\ \hat{u}_2 &= -u_1 \frac{\Delta_2}{L} + u_2 \frac{\Delta_1}{L} \\ \hat{u}_3 &= u_3 \\ \hat{u}_4 &= u_4 \frac{\Delta_1}{L} + u_5 \frac{\Delta_2}{L} \\ \hat{u}_5 &= -u_4 \frac{\Delta_2}{L} + u_5 \frac{\Delta_1}{L} \\ \hat{u}_6 &= u_6 \end{aligned} \right\} T^i = \left[\begin{array}{ccc|cc} \Delta_1/L & \Delta_2/L & 0 & 0 & 0 \\ -\Delta_2/L & \Delta_1/L & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ \hline 0 & 0 & 0 & \Delta_1/L & \Delta_2/L \\ 0 & 0 & 0 & -\Delta_2/L & \Delta_1/L \\ 0 & 0 & 0 & 0 & 1 \end{array} \right] \quad (9.4)$$

Eleman yerel yer değiştirmeleri

Eleman transformasyon matrisi

Eleman genel yer değiştirmeleri

$$\hat{u}^i = T^i u^i = \left[\begin{array}{ccc|ccc} \hat{u}_1 \\ \hat{u}_2 \\ \hat{u}_3 \\ \hat{u}_4 \\ \hat{u}_5 \\ \hat{u}_6 \end{array} \right] = \left[\begin{array}{ccc|ccc} \Delta_1/L & \Delta_2/L & 0 & 0 & 0 & 0 \\ -\Delta_2/L & \Delta_1/L & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ \hline 0 & 0 & 0 & \Delta_1/L & \Delta_2/L & 0 \\ 0 & 0 & 0 & -\Delta_2/L & \Delta_1/L & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{array} \right] \left[\begin{array}{c} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \end{array} \right] \quad (9.5)$$

Eleman genel eşdeğer kuvvetleri

Eleman transformasyon matrisinin transpozu

Eleman yerel eşdeğer kuvvetleri

$$\bar{s}^i = (T^i)^T \hat{s}^i = \left[\begin{array}{c} \bar{s}_1 \\ \bar{s}_2 \\ \bar{s}_3 \\ \bar{s}_4 \\ \bar{s}_5 \\ \bar{s}_6 \end{array} \right] = \left[\begin{array}{ccc|ccc} \Delta_1/L & -\Delta_2/L & 0 & 0 & 0 & 0 \\ \Delta_2/L & \Delta_1/L & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ \hline 0 & 0 & 0 & \Delta_1/L & -\Delta_2/L & 0 \\ 0 & 0 & 0 & \Delta_2/L & \Delta_1/L & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{array} \right] \left[\begin{array}{c} \hat{s}_1 \\ \hat{s}_2 \\ \hat{s}_3 \\ \hat{s}_4 \\ \hat{s}_5 \\ \hat{s}_6 \end{array} \right] \quad (9.6)$$

9.3 Düzlem çerçeve elemanın genel rijitlik matrisi

$$k^i = (T^i)^T \hat{k}^i T^i \quad (9.7)$$

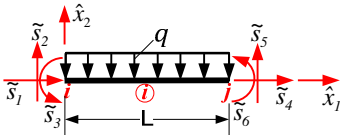
$$k^i = \left[\begin{array}{ccc|ccc} \frac{EA}{L^3} \Delta_1^2 + 12 \frac{EI_3}{L^5} \Delta_2^2 & & & & & \\ \left(\frac{EA}{L^3} - 12 \frac{EI_3}{L^5} \right) \Delta_1 \Delta_2 & \frac{EA}{L^3} \Delta_2^2 + 12 \frac{EI_3}{L^5} \Delta_1^2 & & & & \\ -6 \frac{EI_3}{L^3} \Delta_2 & 6 \frac{EI_3}{L^3} \Delta_1 & 4 \frac{EI_3}{L} & & & \\ \hline - \left(\frac{EA}{L^3} \Delta_1^2 + 12 \frac{EI_3}{L^5} \Delta_2^2 \right) & - \left(\frac{EA}{L^3} - 12 \frac{EI_3}{L^5} \right) \Delta_1 \Delta_2 & 6 \frac{EI_3}{L^3} \Delta_2 & \frac{EA}{L^3} \Delta_1^2 + 12 \frac{EI_3}{L^5} \Delta_2^2 & & \\ - \left(\frac{EA}{L^3} - 12 \frac{EI_3}{L^5} \right) \Delta_1 \Delta_2 & - \left(\frac{EA}{L^3} \Delta_2^2 + 12 \frac{EI_3}{L^5} \Delta_1^2 \right) & -6 \frac{EI_3}{L^3} \Delta_1 & \left(\frac{EA}{L^3} - 12 \frac{EI_3}{L^5} \right) \Delta_1 \Delta_2 & \frac{EA}{L^3} \Delta_2^2 + 12 \frac{EI_3}{L^5} \Delta_1^2 & \\ -6 \frac{EI_3}{L^3} \Delta_2 & 6 \frac{EI_3}{L^3} \Delta_1 & 2 \frac{EI_3}{L} & 6 \frac{EI_3}{L^3} \Delta_2 & -6 \frac{EI_3}{L^3} \Delta_1 & 4 \frac{EI_3}{L} \end{array} \right] \quad (9.8)$$

Simetrik

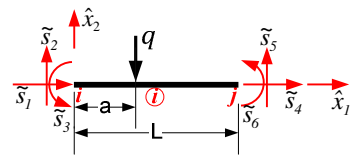
9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

9.4 Yüklü elemanın eşdeğer düğüm yükleri

Eleman üzerindeki dış yüklerin enerji eşdeğerleri sistem düğümlerine aktarılır. Tekil ve düzgün yayılı yükün eşdeğer yükleri (ankastrelik kuvvetleri) aşağıda verilmiştir. Diğer yük tiplerinin eşdeğer yükleri EK3 den veya yapı statikliği kitaplarından alınabilir.

$$\underline{\tilde{s}}^i = \begin{bmatrix} \tilde{s}_1 \\ \tilde{s}_2 \\ \tilde{s}_3 \\ \tilde{s}_4 \\ \tilde{s}_5 \\ \tilde{s}_6 \\ \underline{\tilde{s}}^i \end{bmatrix} = \begin{bmatrix} 0 \\ \frac{qL}{2} \\ \frac{qL^2}{12} \\ 0 \\ \frac{qL}{2} \\ -\frac{qL^2}{12} \end{bmatrix}$$


Şekil 9.2 eşdeğer kuvvetler

$$\underline{\tilde{s}}^i = \begin{bmatrix} \tilde{s}_1 \\ \tilde{s}_2 \\ \tilde{s}_3 \\ \tilde{s}_4 \\ \tilde{s}_5 \\ \tilde{s}_6 \\ \underline{\tilde{s}}^i \end{bmatrix} = \begin{bmatrix} 0 \\ 1 - \frac{3a^2}{L^2} + \frac{2a^3}{L^3} \\ a - \frac{2a^2}{L} + \frac{a^3}{L^2} \\ 0 \\ \frac{3a^2}{L^2} - \frac{2a^3}{L^3} \\ -\frac{a^2}{L} + \frac{a^3}{L^2} \end{bmatrix} q$$


Şekil 9.3 eşdeğer kuvvetler

Eşdeğer yükler yerel koordinatlarda verilmiştir. Eleman yatay, düşey veya eğimli olabileceğinden, sistemin düğüm noktalarına aktarılmadan önce 9.6 bağıntısı ile genel koordinat eksenlerine dönüştürülmesi gerekir.

Sayısal örnek 9.1:

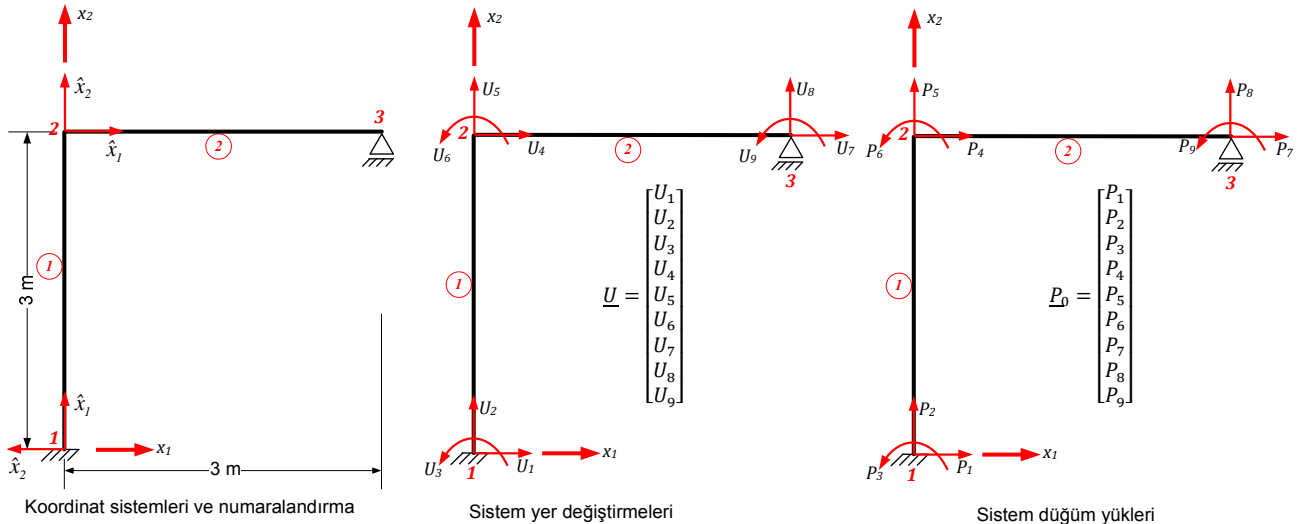
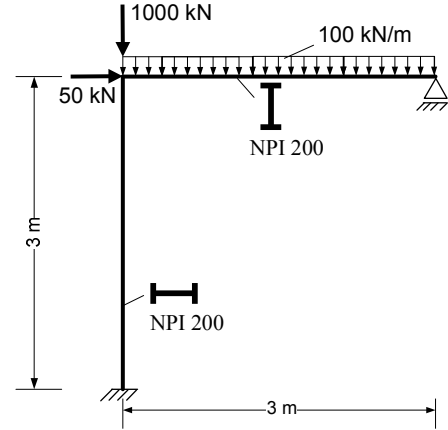
Sağda görülen çerçeve sistem NPI 200 çelik profili ile inşa edilecektir. Kesme, moment ve normal kuvvet diyagramlarını çiziniz.

HAZIRLIK:

Sistem 2 elemanla modellenmiştir. Seçilen koordinat sistemleri, numaralandırma, düğüm yer değiştirmelerinin ve yüklerin adları şekil 9.4 de verilmiştir. 2 nolu elemanın yayılı yük eşdeğeri sistem düğümlerine aktarılacaktır.

Hesaplarda kN ve m birimlerini kullanalım. NPI 200 için elastisite modülü: $E=2.1 \cdot 10^5 \text{ N/mm}^2$ (yapı çeliği için) $=21 \cdot 10^7 \text{ kN/m}^2$, Kesit alanı: $A=33.4 \text{ cm}^2=334 \cdot 10^{-5} \text{ m}^2$, Atalet momenti: $I_3=2140 \text{ cm}^4=214 \cdot 10^{-7} \text{ m}^4$ (çelik profil tablosundan)

Düğüm serbestlik derecesi (bir yatay, bir düşey yer değiştirme, bir dönme) = 3, Sistem serbestlik derecesi = $3 \cdot 3 = 9$



Şekil 9.4: Sistemin modellenmesi

El hesaplarını kolaylaştırmak için aşağıdaki çizelgeyi hazırlamak yararlıdır. Birimler kN ve m dir.

Eleman	E	A	I ₃	i ucu	j ucu	Koordinatlar		Δ ₁	Δ ₂	L	EA/L	EI ₃ /L	A ₁ /L	A ₂ /L
						i	j							
1	21·10 ⁷	334·10 ⁻⁵	214·10 ⁻⁷	1	2	0, 0	0, 3	0	3	3	233800	1498	0	1
2	21·10 ⁷	334·10 ⁻⁵	214·10 ⁻⁷	2	3	0, 3	3, 3	3	0	3	233800	1498	1	0

9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

Elemanların transformasyon matrisleri: **Bak 9.4**

$$\underline{T}^1 = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}, \quad \underline{T}^2 = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

Elemanların yerel rijitlik matrisleri: **Bak 9.1**

$$\hat{k}^1 = \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \left[\begin{array}{ccc|ccc} 233800 & 0 & 0 & -233800 & 0 & 0 \\ 0 & 1997 & 2996 & 0 & -1997 & 2996 \\ 0 & 2996 & 5992 & 0 & -2996 & 2996 \\ \hline -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{array} \right]$$

$$\hat{k}^2 = \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \left[\begin{array}{ccc|ccc} 233800 & 0 & 0 & -233800 & 0 & 0 \\ 0 & 1997 & 2996 & 0 & -1997 & 2996 \\ 0 & 2996 & 5992 & 0 & -2996 & 2996 \\ \hline -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{array} \right]$$

Elemanların genel rijitlik matrisleri ve sistem rijitlik matrisi: $\underline{k}^i = (\underline{T}^i)^T \hat{k}^i \underline{T}^i$

$$\underline{k}^1 = \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \left[\begin{array}{ccc|ccc} 0 & -1 & 0 & 0 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{array} \right] \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \left[\begin{array}{ccc|ccc} 233800 & 0 & 0 & -233800 & 0 & 0 \\ 0 & 1997 & 2996 & 0 & -1997 & 2996 \\ 0 & 2996 & 5992 & 0 & -2996 & 2996 \\ \hline -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{array} \right] \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \left[\begin{array}{ccc|ccc} 0 & 1 & 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{array} \right]$$

$$\underline{k}^1 = \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \left[\begin{array}{ccc|ccc} 1997 & 0 & -2996 & -1997 & 0 & -2996 \\ 0 & 233800 & 0 & 0 & -233800 & 0 \\ -2996 & 0 & 5992 & 2996 & 0 & 2996 \\ \hline -1997 & 0 & 2996 & 1997 & 0 & 2996 \\ 0 & -233800 & 0 & 0 & 233800 & 0 \\ -2996 & 0 & 2996 & 2996 & 0 & 5992 \end{array} \right]$$

$$\underline{k}^2 = (\underline{T}^2)^T \hat{k}^2 \underline{T}^2 = \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \left[\begin{array}{ccc|ccc} 233800 & 0 & 0 & -233800 & 0 & 0 \\ 0 & 1997 & 2996 & 0 & -1997 & 2996 \\ 0 & 2996 & 5992 & 0 & -2996 & 2996 \\ \hline -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{array} \right]$$

T^2 birim matris olduğundan çarpımı yapmaya gerek yoktur, $\underline{k}^2 = \hat{k}^2$ dir.

$$\underline{K}_D = \begin{array}{c} \mathbf{1} \\ \mathbf{2} \\ \mathbf{3} \end{array} \begin{array}{c} \mathbf{1} \\ \mathbf{2} \\ \mathbf{3} \end{array} \left[\begin{array}{ccc|ccc|ccc} 1997 & 0 & -2996 & -1997 & 0 & -2996 & 0 & 0 & 0 \\ 0 & 233800 & 0 & 0 & -233800 & 0 & 0 & 0 & 0 \\ -2996 & 0 & 5992 & 2996 & 0 & 2996 & 0 & 0 & 0 \\ \hline -1997 & 0 & 2996 & 235797 & 0 & 2996 & -233800 & 0 & 0 \\ 0 & -233800 & 0 & 0 & 235797 & 2996 & 0 & -1997 & 2996 \\ -2996 & 0 & 2996 & 2996 & 2996 & 11984 & 0 & -2996 & 2996 \\ \hline 0 & 0 & 0 & -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 0 & 0 & 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{array} \right]$$

Sistem rijitlik matrisi

Eleman eşdeğer yükleri:

$$\underline{\tilde{s}}^1 = \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \left[\begin{array}{c} \tilde{s}_1 \\ \tilde{s}_2 \\ \tilde{s}_3 \\ \tilde{s}_4 \\ \tilde{s}_5 \\ \tilde{s}_6 \end{array} \right] = \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \left[\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array} \right] \xrightarrow{\text{DÖNÜŞTÜR}} \underline{\tilde{s}}^1 = (\underline{T}^1)^T \underline{\tilde{s}}^1 = \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \left[\begin{array}{c} \tilde{s}_1 \\ \tilde{s}_2 \\ \tilde{s}_3 \\ \tilde{s}_4 \\ \tilde{s}_5 \\ \tilde{s}_6 \end{array} \right] = \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \begin{array}{c} \mathbf{1} \\ \mathbf{2} \end{array} \left[\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{array} \right]$$

1. eleman üzerinde yük yok

$$\underline{\tilde{s}}^2 = \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \left[\begin{array}{c} \tilde{s}_1 \\ \tilde{s}_2 \\ \tilde{s}_3 \\ \tilde{s}_4 \\ \tilde{s}_5 \\ \tilde{s}_6 \end{array} \right] = \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \left[\begin{array}{c} 0 \\ 150 \\ 75 \\ 0 \\ 150 \\ -75 \end{array} \right] \xrightarrow{\text{DÖNÜŞTÜR}} \underline{\tilde{s}}^2 = (\underline{T}^2)^T \underline{\tilde{s}}^2 = \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \left[\begin{array}{c} \tilde{s}_1 \\ \tilde{s}_2 \\ \tilde{s}_3 \\ \tilde{s}_4 \\ \tilde{s}_5 \\ \tilde{s}_6 \end{array} \right] = \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \begin{array}{c} \mathbf{2} \\ \mathbf{3} \end{array} \left[\begin{array}{c} 0 \\ 150 \\ 75 \\ 0 \\ 150 \\ -75 \end{array} \right]$$

2. elemanın düzgün yayılı yükünün yerel eşdeğer tekil yükleri. Bak şekil 9.2

Yerel eşdeğer kuvvetlerin genel eşdeğer yüklerle dönüştürülmesi, Bak: 9.6. T^2 birim matris olduğundan $\underline{\tilde{s}}^2 = \underline{\tilde{s}}^2$ dir.

9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

Sistem yük vektörü:

$$P_0 = \begin{bmatrix} P_1 \\ P_2 \\ P_3 \\ P_4 \\ P_5 \\ P_6 \\ P_7 \\ P_8 \\ P_9 \end{bmatrix} = \begin{bmatrix} P_1 \\ P_2 \\ P_3 \\ 50 \\ -1000 \\ 0 \\ 0 \\ P_8 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ -150 \\ -75 \\ -150 \\ 0 \\ -150 \\ 75 \end{bmatrix} = \begin{bmatrix} P_1 \\ P_2 \\ P_3 \\ 50 \\ -1150 \\ -75 \\ 0 \\ P_8 - 150 \\ 75 \end{bmatrix}$$

Düğümde toplam yük.
P₁, P₂, P₃, P₈: Reaksiyonlar

Düğümde verilmiş yükler ve reaksiyonlar

P_{esdeğer}

Sistem denge koşulu: $K_0 U = P_0$

$$\begin{bmatrix} 1997 & 0 & -2996 & -1997 & 0 & -2996 & 0 & 0 & 0 \\ 0 & 233800 & 0 & 0 & -233800 & 0 & 0 & 0 & 0 \\ -2996 & 0 & 5992 & 2996 & 0 & 2996 & 0 & 0 & 0 \\ -1997 & 0 & 2996 & 235797 & 0 & 2996 & -233800 & 0 & 0 \\ 0 & -233800 & 0 & 0 & 235797 & 2996 & 0 & -1997 & 2996 \\ -2996 & 0 & 2996 & 2996 & 2996 & 11984 & 0 & -2996 & 2996 \\ 0 & 0 & 0 & -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 0 & 0 & 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{bmatrix} \begin{bmatrix} U_1 \\ U_2 \\ U_3 \\ U_4 \\ U_5 \\ U_6 \\ U_7 \\ U_8 \\ U_9 \end{bmatrix} = \begin{bmatrix} P_1 \\ P_2 \\ P_3 \\ 50 \\ -1150 \\ -75 \\ 0 \\ P_8 - 150 \\ 75 \end{bmatrix}$$

K₀

u

P₀

Sınır koşulları ve işlenmesi: $1 \cdot U_1 = 0$, $1 \cdot U_2 = 0$, $1 \cdot U_3 = 0$, $1 \cdot U_8 = 0$

$$\begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 235797 & 0 & 2996 & -233800 & 0 & 0 \\ 0 & 0 & 0 & 0 & 235797 & 2996 & 0 & -1997 & 2996 \\ 0 & 0 & 0 & 2996 & 2996 & 11984 & 0 & 0 & 2996 \\ 0 & 0 & 0 & -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 2996 & 2996 & 0 & 0 & 5992 \end{bmatrix} \begin{bmatrix} U_1 \\ U_2 \\ U_3 \\ U_4 \\ U_5 \\ U_6 \\ U_7 \\ U_8 \\ U_9 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 50 \\ -1150 \\ -75 \\ 0 \\ 0 \\ 75 \end{bmatrix}$$

K

u

P

ÇÖZÜM

$$\begin{bmatrix} U_1 \\ U_2 \\ U_3 \\ U_4 \\ U_5 \\ U_6 \\ U_7 \\ U_8 \\ U_9 \end{bmatrix} = \begin{bmatrix} 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \\ 0.070163 \text{ m} \\ -0.004876 \text{ m} \\ -0.030079 \text{ rad} \\ 0.070163 \text{ m} \\ 0 \text{ m} \\ 0.029994 \text{ rad} \end{bmatrix}$$

u

u

Denge kontrolü ve reaksiyonlar: $P_{hesap} = K_0 U - P_{esdeğer}$

$$\begin{bmatrix} 1997 & 0 & -2996 & -1997 & 0 & -2996 & 0 & 0 & 0 \\ 0 & 233800 & 0 & 0 & -233800 & 0 & 0 & 0 & 0 \\ -2996 & 0 & 5992 & 2996 & 0 & 2996 & 0 & 0 & 0 \\ -1997 & 0 & 2996 & 235797 & 0 & 2996 & -233800 & 0 & 0 \\ 0 & -233800 & 0 & 0 & 235797 & 2996 & 0 & -1997 & 2996 \\ -2996 & 0 & 2996 & 2996 & 2996 & 11984 & 0 & -2996 & 2996 \\ 0 & 0 & 0 & -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 0 & 0 & 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{bmatrix} \begin{bmatrix} 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \\ 0.070163 \text{ m} \\ -0.004876 \text{ m} \\ -0.030079 \text{ rad} \\ 0.070163 \text{ m} \\ 0 \text{ m} \\ 0.029994 \text{ rad} \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ 0 \\ -150 \\ -75 \\ -150 \\ 75 \end{bmatrix} = \begin{bmatrix} -50 \text{ kN} \\ 1140 \text{ kN} \\ 120 \text{ kNm} \\ 50 \text{ kN} \\ -1000 \text{ kN} \\ 0 \text{ kNm} \\ 0 \text{ kNm} \\ 150 \text{ kN} \\ 0 \text{ kNm} \end{bmatrix}$$

K₀

u

P_{esdeğer}

P_{hesap}

Reaksiyon

Reaksiyon

Reaksiyon

Reaksiyon

Reaksiyon

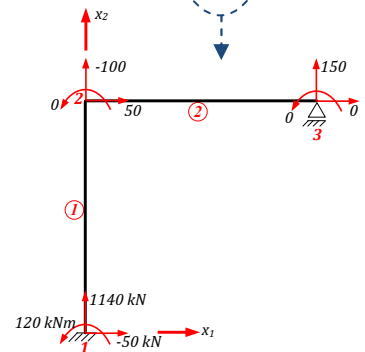
Reaksiyon

Elemanların genel yer değiştirmeleri:

$$\underline{u}^1 = \begin{bmatrix} 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \\ 0.070163 \text{ m} \\ -0.004876 \text{ m} \\ -0.030079 \text{ rad} \end{bmatrix}, \quad \underline{u}^2 = \begin{bmatrix} 0.070163 \text{ m} \\ -0.004876 \text{ m} \\ -0.030079 \text{ rad} \\ 0.070163 \text{ m} \\ 0 \text{ m} \\ 0.029994 \text{ rad} \end{bmatrix}$$

u¹

u²



9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

Elemanların yerel yer değiştirmeleri: $\hat{u}^i = T^i u^i$ Bak 9.5

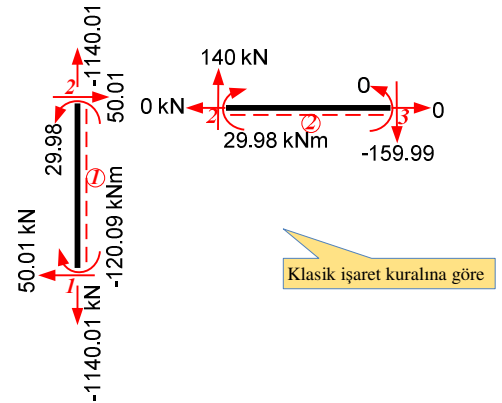
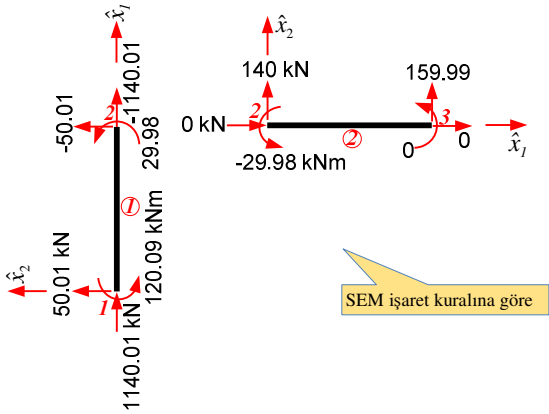
$$\hat{u}^1 = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \\ 0.070163 \text{ m} \\ -0.004876 \text{ m} \\ -0.030079 \text{ rad} \end{bmatrix} = \begin{bmatrix} 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \\ -0.004876 \text{ m} \\ -0.070163 \text{ m} \\ -0.030079 \text{ rad} \end{bmatrix}$$

$$\hat{u}^2 = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0.070163 \text{ m} \\ -0.004876 \text{ m} \\ -0.030079 \text{ rad} \\ 0.070163 \text{ m} \\ 0 \text{ m} \\ 0.029994 \text{ rad} \end{bmatrix} = \begin{bmatrix} 0.070163 \text{ m} \\ -0.004876 \text{ m} \\ -0.030079 \text{ rad} \\ 0.070163 \text{ m} \\ 0 \text{ m} \\ 0.029994 \text{ rad} \end{bmatrix}$$

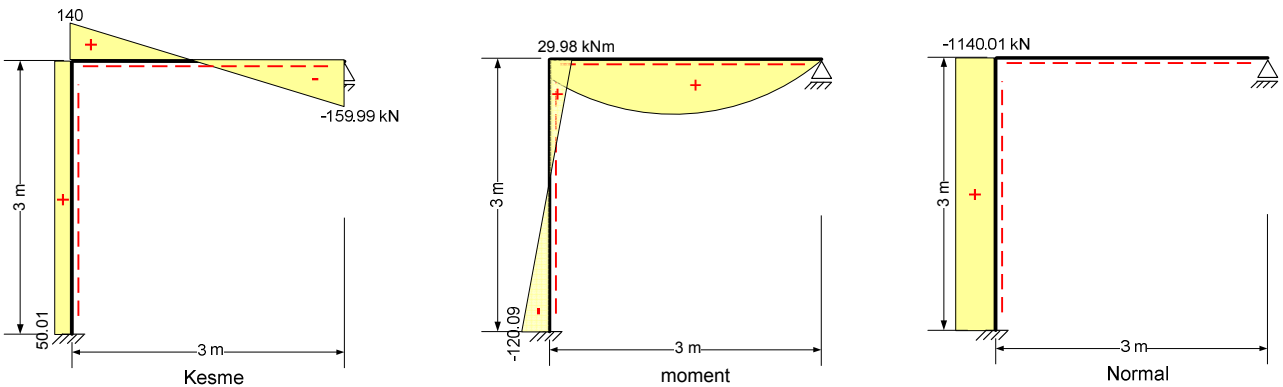
Elemanların yerel kuvvetleri: $\hat{k}^i \hat{u}^i + \hat{s}^i = \hat{\delta}^i$ Bak 9.2

$$\hat{\delta}^1 = \begin{bmatrix} \hat{\delta}_1 \\ \hat{\delta}_2 \\ \hat{\delta}_3 \\ \hat{\delta}_4 \\ \hat{\delta}_5 \\ \hat{\delta}_6 \end{bmatrix} = \begin{bmatrix} 233800 & 0 & 0 & -233800 & 0 & 0 \\ 0 & 1997 & 2996 & 0 & -1997 & 2996 \\ 0 & 2996 & 5992 & 0 & -2996 & 2996 \\ -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{bmatrix} \begin{bmatrix} 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \\ -0.004876 \text{ m} \\ -0.070163 \text{ m} \\ -0.030079 \text{ rad} \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 1140.01 \text{ kN} \\ 50.01 \text{ kN} \\ 120.09 \text{ kNm} \\ -1140.01 \text{ kN} \\ -50.01 \text{ kN} \\ 29.98 \text{ kNm} \end{bmatrix}$$

$$\hat{\delta}^2 = \begin{bmatrix} \hat{\delta}_1 \\ \hat{\delta}_2 \\ \hat{\delta}_3 \\ \hat{\delta}_4 \\ \hat{\delta}_5 \\ \hat{\delta}_6 \end{bmatrix} = \begin{bmatrix} 233800 & 0 & 0 & -233800 & 0 & 0 \\ 0 & 1997 & 2996 & 0 & -1997 & 2996 \\ 0 & 2996 & 5992 & 0 & -2996 & 2996 \\ -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{bmatrix} \begin{bmatrix} 0.070163 \text{ m} \\ -0.004876 \text{ m} \\ -0.030079 \text{ rad} \\ 0.070163 \text{ m} \\ 0 \text{ m} \\ 0.029994 \text{ rad} \end{bmatrix} + \begin{bmatrix} 0 \\ 150 \\ 75 \\ 150 \\ -75 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \text{ kN} \\ 140 \text{ kN} \\ -29.98 \text{ kNm} \\ 0 \text{ kN} \\ 159.99 \text{ kN} \\ 0 \text{ kNm} \end{bmatrix}$$



Diyagramlar(klasik işaret kuralına göre):



9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

Sayısal örnek 9.2

Sağda görülen çerçeve sistem I 200 profili ile inşa edilecektir. Kesme, moment ve normal kuvvet diyagramlarını çizin.

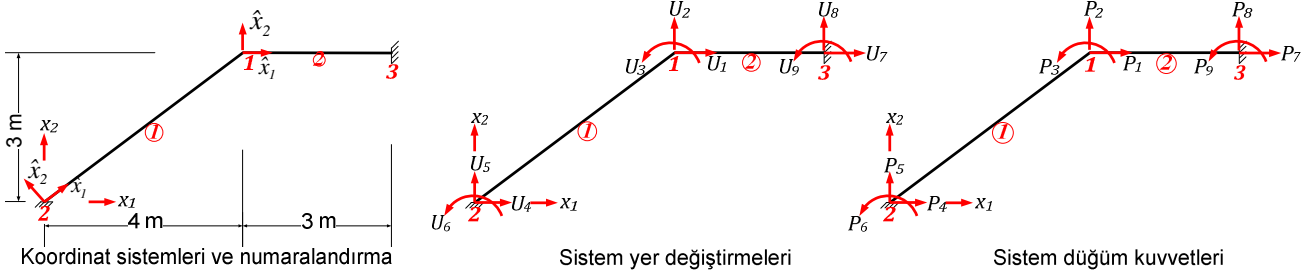
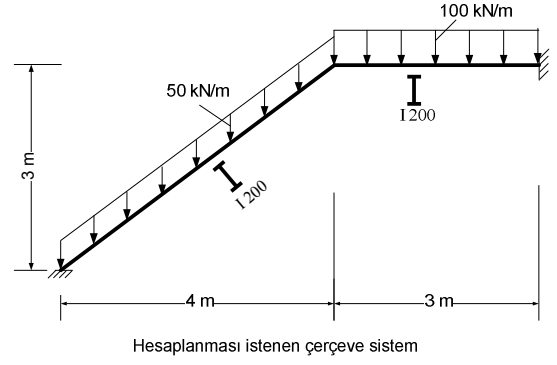
HAZIRLIK:

Sistem için seçilen koordinat sistemleri, numaralandırma, düğüm yer değiştirmelerinin ve yüklerin adları şekil 9.5 de verilmiştir. Sistem 2 elemanla modellenmiştir. Elemanların yayılı yük eşdeğeri sistem düğümlerine aktarılacaktır.

Hesaplarda kN ve m birimlerini kullanalım.

Elastisite modülü: $E=2.1 \cdot 10^5 \text{ N/mm}^2$ (yapı çeliği çin) $=21 \cdot 10^7 \text{ kN/m}^2$
Kesit alanı $A=33.4 \text{ cm}^2=334 \cdot 10^{-5} \text{ m}^2$, Atalet momenti: $I_3=2140 \text{ cm}^2=214 \cdot 10^{-7} \text{ m}^4$ (çelik profil tablosundan)

Düğüm serbestlik derecesi (bir yatay, bir düşey yer değiştirme, bir dönme) = 3, Sistem serbestlik derecesi = $3 \cdot 3 = 9$



El hesaplarını için aşağıdaki çizelgeyi hazırlayalım. Birimler kN ve m dir.

Eleman	E	A	I_3	i ucu	j ucu	Koordinatlar		Δ_1	Δ_2	L	EA/L	EI_3/L	$\frac{\Delta_1}{L}$	$\frac{\Delta_2}{L}$
						i	j							
1	$21 \cdot 10^7$	$334 \cdot 10^{-5}$	$214 \cdot 10^{-7}$	2	1	0, 0	4, 3	4	3	5	140280	898.8	0.8	0.6
2	$21 \cdot 10^7$	$334 \cdot 10^{-5}$	$214 \cdot 10^{-7}$	1	3	4, 3	7, 3	3	0	3	233800	1498	1	0

Elemanların transformasyon matrisleri: Bak 9.4

$$\underline{T}^1 = \begin{bmatrix} 0.8 & 0.6 & 0 & 0 & 0 & 0 \\ -0.6 & 0.8 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.8 & 0.6 & 0 \\ 0 & 0 & 0 & -0.6 & 0.8 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}, \quad \underline{T}^2 = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

Elemanların yerel rijitlik matrisleri: Bak 9.1

$$\underline{k}^1 = \begin{bmatrix} 140280 & 0 & 0 & -140280 & 0 & 0 \\ 0 & 431 & 1079 & 0 & -431 & 1079 \\ 0 & 1079 & 3595 & 0 & -1079 & 1798 \\ -140280 & 0 & 0 & 140280 & 0 & 0 \\ 0 & -431 & -1079 & 0 & 431 & -1079 \\ 0 & 1079 & 1798 & 0 & -1079 & 3595 \end{bmatrix}$$

$$\underline{k}^2 = \begin{bmatrix} 233800 & 0 & 0 & -233800 & 0 & 0 \\ 0 & 1997 & 2996 & 0 & -1997 & 2996 \\ 0 & 2996 & 5992 & 0 & -2996 & 2996 \\ -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{bmatrix}$$

9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

Elemanların genel rijitlik matrisleri ve sistem rijitlik matrisi: $\underline{k}^i = (\underline{T}^i)^T \hat{\underline{k}}^i \underline{T}^i$

$$\underline{k}^1 = \begin{bmatrix} 0.8 & -0.6 & 0 & 0 & 0 & 0 \\ 0.6 & 0.8 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.8 & -0.6 & 0 \\ 0 & 0 & 0 & 0.6 & 0.8 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 140280 & 0 & 0 & -140280 & 0 & 0 \\ 0 & 431 & 1079 & 0 & -431 & 1079 \\ 0 & 1079 & 3595 & 0 & -1079 & 1798 \\ -140280 & 0 & 0 & 140280 & 0 & 0 \\ 0 & -431 & -1079 & 0 & 431 & -1079 \\ 0 & 1079 & 1798 & 0 & -1079 & 3595 \end{bmatrix} \begin{bmatrix} 0.8 & 0.6 & 0 & 0 & 0 & 0 \\ -0.6 & 0.8 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.8 & 0.6 & 0 \\ 0 & 0 & 0 & -0.6 & 0.8 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\underline{k}^1 = \begin{bmatrix} 89935 & 67127 & -647 & -89935 & -67127 & -647 \\ 67127 & 50777 & 863 & -67127 & -50777 & 863 \\ -647 & 863 & 3595 & 647 & -863 & 1798 \\ -89935 & -67127 & 647 & 89935 & 67127 & 647 \\ -67127 & -50777 & -863 & 67127 & 50777 & -863 \\ -647 & 863 & 1798 & 647 & -863 & 3595 \end{bmatrix}$$

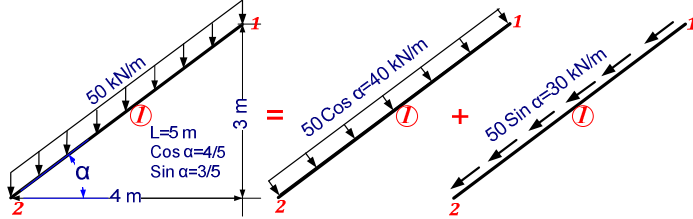
$$\underline{k}^2 = (\underline{T}^2)^T \hat{\underline{k}}^2 \underline{T}^2 = \begin{bmatrix} 233800 & 0 & 0 & -233800 & 0 & 0 \\ 0 & 1997 & 2996 & 0 & -1997 & 2996 \\ 0 & 2996 & 5992 & 0 & -2996 & 2996 \\ -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{bmatrix}$$

\underline{T}^2 birim matris olduğundan çarpımı yapmaya gerek yoktur, $\underline{k}^2 = \hat{\underline{k}}^2$ dir.

$$\underline{K}_D = \begin{bmatrix} 323735 & 67127 & 647 & -89935 & -67127 & 647 & -233800 & 0 & 0 \\ 67127 & 52774 & 2133 & -67127 & -50777 & -863 & 0 & -1997 & 2996 \\ 647 & 2133 & 9587 & -647 & 863 & 1798 & 0 & -2996 & 2996 \\ -89935 & -67127 & -647 & 89935 & 67127 & -647 & 0 & 0 & 0 \\ -67127 & -50777 & 863 & 67127 & 50777 & 863 & 0 & 0 & 0 \\ 647 & -863 & 1798 & -647 & 863 & 3595 & 0 & 0 & 0 \\ -233800 & 0 & 0 & 0 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 0 & 0 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & 0 & 0 & 0 & -2996 & 5992 \end{bmatrix}$$

Sistem rijitlik matrisi

Eleman eşdeğer yerel ve genel yükleri:



1. elemanın düzgün yayılı yükünün yerel eşdeğer tekil yükleri. Bak: EK3

$$\underline{\bar{s}}^1 = \begin{bmatrix} \bar{s}_1 \\ \bar{s}_2 \\ \bar{s}_3 \\ \bar{s}_4 \\ \bar{s}_5 \\ \bar{s}_6 \end{bmatrix} = \begin{bmatrix} 0 \\ 100 \\ 83.33 \\ 0 \\ 100 \\ -83.33 \end{bmatrix} + \begin{bmatrix} 75 \\ 0 \\ 0 \\ 75 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 75 \\ 100 \\ 83.33 \\ 75 \\ 100 \\ -83.33 \end{bmatrix}$$

$$\underline{\bar{s}}^1 = \begin{bmatrix} \bar{s}_1 \\ \bar{s}_2 \\ \bar{s}_3 \\ \bar{s}_4 \\ \bar{s}_5 \\ \bar{s}_6 \end{bmatrix} = \begin{bmatrix} 75 \\ 100 \\ 83.33 \\ 75 \\ 100 \\ -83.33 \end{bmatrix}$$

DÖNÜŞTÜR

$$\underline{\bar{s}}^1 = (\underline{T}^1)^T \underline{\bar{s}}^1 = \begin{bmatrix} \bar{s}_1 \\ \bar{s}_2 \\ \bar{s}_3 \\ \bar{s}_4 \\ \bar{s}_5 \\ \bar{s}_6 \end{bmatrix} = \begin{bmatrix} 0.8 & -0.6 & 0 & 0 & 0 & 0 \\ 0.6 & 0.8 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.8 & -0.6 & 0 \\ 0 & 0 & 0 & 0.6 & 0.8 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 75 \\ 100 \\ 83.33 \\ 75 \\ 100 \\ -83.33 \end{bmatrix} = \begin{bmatrix} 0 \\ 125 \\ 83.33 \\ 0 \\ 125 \\ -83.33 \end{bmatrix}$$

Bak: 9.6

$$\underline{\bar{s}}^2 = \begin{bmatrix} \bar{s}_1 \\ \bar{s}_2 \\ \bar{s}_3 \\ \bar{s}_4 \\ \bar{s}_5 \\ \bar{s}_6 \end{bmatrix} = \begin{bmatrix} 0 \\ 150 \\ 75 \\ 0 \\ 150 \\ -75 \end{bmatrix}$$

DÖNÜŞTÜR

$$\underline{\bar{s}}^2 = (\underline{T}^2)^T \underline{\bar{s}}^2 = \begin{bmatrix} \bar{s}_1 \\ \bar{s}_2 \\ \bar{s}_3 \\ \bar{s}_4 \\ \bar{s}_5 \\ \bar{s}_6 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ 150 \\ 75 \\ 0 \\ 150 \\ -75 \end{bmatrix} = \begin{bmatrix} 0 \\ 150 \\ 75 \\ 0 \\ 150 \\ -75 \end{bmatrix}$$

Sistem yük vektörü:

$$\underline{P}_0 = \begin{bmatrix} P_1 \\ P_2 \\ P_3 \\ P_4 \\ P_5 \\ P_6 \\ P_7 \\ P_8 \\ P_9 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -125 \\ -83.33 \\ 0 \\ -150 \\ 75 \end{bmatrix} + \begin{bmatrix} 0 \\ -275 \\ 8.33 \\ 0 \\ -125 \\ -83.33 \\ 0 \\ -150 \\ 75 \end{bmatrix} = \begin{bmatrix} 0 \\ -275 \\ 8.33 \\ 0 \\ -125 \\ -83.33 \\ 0 \\ -150 \\ 75 \end{bmatrix}$$

$$\underline{P}_0 = \begin{bmatrix} P_1 \\ P_2 \\ P_3 \\ P_4 \\ P_5 \\ P_6 \\ P_7 \\ P_8 \\ P_9 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -125 \\ -83.33 \\ 0 \\ -150 \\ 75 \end{bmatrix} + \begin{bmatrix} 0 \\ -275 \\ 8.33 \\ 0 \\ -125 \\ -83.33 \\ 0 \\ -150 \\ 75 \end{bmatrix} = \begin{bmatrix} 0 \\ -275 \\ 8.33 \\ 0 \\ -125 \\ -83.33 \\ 0 \\ -150 \\ 75 \end{bmatrix}$$

Düğümelerde toplam yük. $P_4, P_5, P_6, P_7, P_8, P_9$: Reaksiyonlar

Düğümelerde verilmiş yükler ve reaksiyonlar

9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

Sistem denge koşulu: $K_0 \underline{U} = \underline{P}_0$

$$\begin{array}{c}
 \mathbf{1} \\
 \mathbf{2} \\
 \mathbf{3}
 \end{array}
 \begin{array}{ccc|ccc|ccc}
 323735 & 67127 & 647 & -89935 & -67127 & 647 & -233800 & 0 & 0 \\
 67127 & 52774 & 2133 & -67127 & -50777 & -863 & 0 & -1997 & 2996 \\
 647 & 2133 & 9587 & -647 & 863 & 1798 & 0 & -2996 & 2996 \\
 \hline
 -89935 & -67127 & -647 & 89935 & 67127 & -647 & 0 & 0 & 0 \\
 -67127 & -50777 & 863 & 67127 & 50777 & 863 & 0 & 0 & 0 \\
 647 & -863 & 1798 & -647 & 863 & 3595 & 0 & 0 & 0 \\
 \hline
 -233000 & 0 & 0 & 0 & 0 & 0 & 233800 & 0 & 0 \\
 0 & -1997 & -2996 & 0 & 0 & 0 & 0 & 1997 & -2996 \\
 0 & 2996 & 2996 & 0 & 0 & 0 & 0 & -2996 & 5992
 \end{array}
 \begin{array}{c}
 U_1 \\
 U_2 \\
 U_3 \\
 U_4 \\
 U_5 \\
 U_6 \\
 U_7 \\
 U_8 \\
 U_9
 \end{array}
 =
 \begin{array}{c}
 0 \\
 -275 \\
 8.33 \\
 P_4 \\
 P_5 - 125 \\
 P_6 - 83.33 \\
 P_7 \\
 P_8 - 150 \\
 P_9 + 75
 \end{array}$$

Sınır koşulları ve işlenmesi: $1 \cdot U_3 = 0$, $1 \cdot U_4 = 0$, $1 \cdot U_5 = 0$, $1 \cdot U_6 = 0$, $1 \cdot U_7 = 0$, $1 \cdot U_8 = 0$

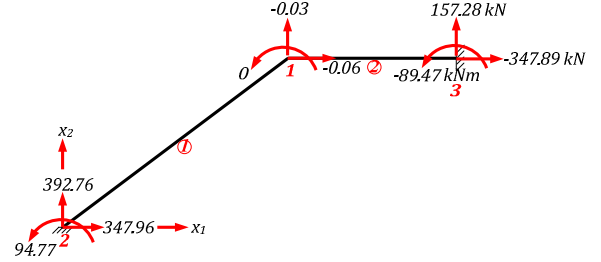
$$\begin{array}{c}
 \mathbf{1} \\
 \mathbf{2} \\
 \mathbf{3}
 \end{array}
 \begin{array}{ccc|ccc|ccc}
 323735 & 67127 & 647 & 0 & 0 & 0 & 0 & 0 & 0 \\
 67127 & 52774 & 2133 & 0 & 0 & 0 & 0 & 0 & 0 \\
 647 & 2133 & 9587 & 0 & 0 & 0 & 0 & 0 & 0 \\
 \hline
 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 & 0 \\
 \hline
 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 1
 \end{array}
 \begin{array}{c}
 U_1 \\
 U_2 \\
 U_3 \\
 U_4 \\
 U_5 \\
 U_6 \\
 U_7 \\
 U_8 \\
 U_9
 \end{array}
 =
 \begin{array}{c}
 0 \\
 -275 \\
 8.33 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0 \\
 0
 \end{array}
 \xrightarrow{\text{ÇÖZÜM}}
 \begin{array}{c}
 U_1 \\
 U_2 \\
 U_3 \\
 U_4 \\
 U_5 \\
 U_6 \\
 U_7 \\
 U_8 \\
 U_9
 \end{array}
 =
 \begin{array}{c}
 0.001488 \text{ m} \\
 -0.007200 \text{ m} \\
 0.002370 \text{ rad} \\
 0 \text{ m} \\
 0 \text{ m} \\
 0 \text{ rad} \\
 0 \text{ m} \\
 0 \text{ m} \\
 0 \text{ rad}
 \end{array}$$

Denge kontrolü ve reaksiyonlar: $\underline{P}_{\text{hesap}} = \underline{K}_0 \underline{U} - \underline{P}_{\text{eşdeğer}}$

$$\begin{array}{c}
 \mathbf{1} \\
 \mathbf{2} \\
 \mathbf{3}
 \end{array}
 \begin{array}{ccc|ccc|ccc}
 323735 & 67127 & 647 & -89935 & -67127 & 647 & -233800 & 0 & 0 \\
 67127 & 52774 & 2133 & -67127 & -50777 & -863 & 0 & -1997 & 2996 \\
 647 & 2133 & 9587 & -647 & 863 & 1798 & 0 & -2996 & 2996 \\
 \hline
 -89935 & -67127 & -647 & 89935 & 67127 & -647 & 0 & 0 & 0 \\
 -67127 & -50777 & 863 & 67127 & 50777 & 863 & 0 & 0 & 0 \\
 647 & -863 & 1798 & -647 & 863 & 3595 & 0 & 0 & 0 \\
 \hline
 -233000 & 0 & 0 & 0 & 0 & 0 & 233800 & 0 & 0 \\
 0 & -1997 & -2996 & 0 & 0 & 0 & 0 & 1997 & -2996 \\
 0 & 2996 & 2996 & 0 & 0 & 0 & 0 & -2996 & 5992
 \end{array}
 \begin{array}{c}
 0.001488 \text{ m} \\
 -0.007200 \text{ m} \\
 0.002370 \text{ rad} \\
 0 \text{ m} \\
 0 \text{ m} \\
 0 \text{ rad} \\
 0 \text{ m} \\
 0 \text{ m} \\
 0 \text{ rad}
 \end{array}
 -
 \begin{array}{c}
 0 \\
 -275 \\
 8.33 \\
 0 \\
 -125 \\
 -83.33 \\
 0 \\
 -150 \\
 75
 \end{array}
 =
 \begin{array}{c}
 -0.06 \text{ kN} \\
 -0.03 \text{ kN} \\
 0 \text{ rad} \\
 347.96 \text{ kN} \\
 392.76 \text{ kN} \\
 94.77 \text{ kNm} \\
 -347.89 \text{ kN} \\
 157.28 \text{ kN} \\
 -89.47 \text{ kNm}
 \end{array}$$

Elemanların genel yer değiştirmeleri:

$$\underline{u}^1 = \begin{bmatrix} 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \\ 0.001488 \text{ m} \\ -0.007200 \text{ m} \\ -0.002370 \text{ rad} \end{bmatrix}, \quad \underline{u}^2 = \begin{bmatrix} 0.001488 \text{ m} \\ -0.007200 \text{ m} \\ -0.002370 \text{ rad} \\ 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \end{bmatrix}$$



Elemanların yerel yer değiştirmeleri: $\hat{u}^i = T^i \underline{u}^i$ (Bak: 9.5)

$$\underline{\hat{u}}^1 = \begin{bmatrix} 0.8 & 0.6 & 0 & 0 & 0 & 0 \\ -0.6 & 0.8 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0.8 & 0.6 & 0 \\ 0 & 0 & 0 & -0.6 & 0.8 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}
 \begin{bmatrix} 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \\ 0.001488 \text{ m} \\ -0.007200 \text{ m} \\ -0.002370 \text{ rad} \end{bmatrix}
 =
 \begin{bmatrix} 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \\ -0.003130 \text{ m} \\ -0.006653 \text{ m} \\ -0.002370 \text{ rad} \end{bmatrix}$$

$$\underline{\hat{u}}^2 = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}
 \begin{bmatrix} 0.001488 \text{ m} \\ -0.007200 \text{ m} \\ -0.002370 \text{ rad} \\ 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \end{bmatrix}
 =
 \begin{bmatrix} 0.001488 \text{ m} \\ -0.007200 \text{ m} \\ -0.002370 \text{ rad} \\ 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \end{bmatrix}$$

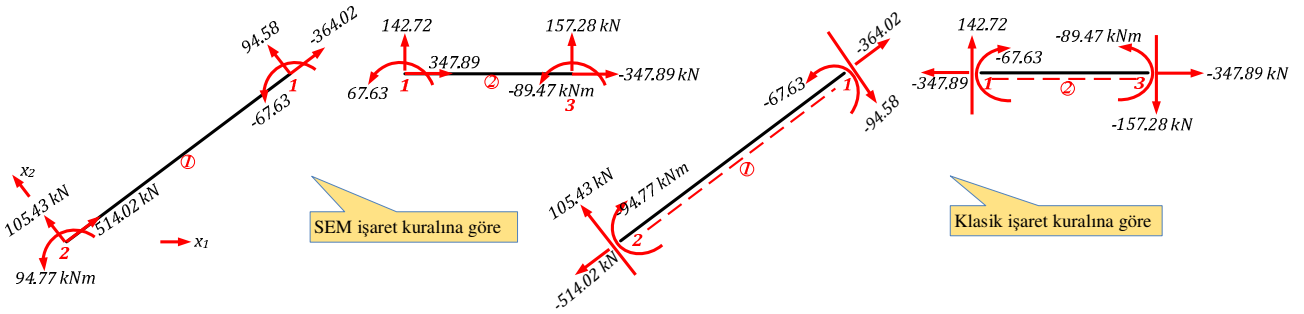
Hesaplanan reaksiyonlar ve düğüm kuvvetleri

9. Düzlem çerçeve elemanı rijitlik ve transformasyon matrisi

Elemanların yerel kuvvetleri: $\hat{k}^i \hat{u}^i + \bar{s}^i = \hat{s}^i$ Bak 9.2

$$\hat{s}^1 = \begin{bmatrix} \hat{s}_1 \\ \hat{s}_2 \\ \hat{s}_3 \\ \hat{s}_4 \\ \hat{s}_5 \\ \hat{s}_6 \end{bmatrix} = \begin{bmatrix} 140280 & 0 & 0 & -140280 & 0 & 0 \\ 0 & 431 & 1079 & 0 & -431 & 1079 \\ 0 & 1079 & 3595 & 0 & -1079 & 1798 \\ -140280 & 0 & 0 & 140280 & 0 & 0 \\ 0 & -431 & -1079 & 0 & 431 & -1079 \\ 0 & 1079 & 1798 & 0 & -1079 & 3595 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ -0.003130 \text{ m} \\ -0.006653 \text{ m} \\ -0.002370 \text{ rad} \end{bmatrix} + \begin{bmatrix} 75 \\ 100 \\ 83.33 \\ 75 \\ 100 \\ -83.33 \end{bmatrix} = \begin{bmatrix} 514.02 \text{ kN} \\ 105.43 \text{ kN} \\ 94.77 \text{ kNm} \\ -364.02 \text{ kN} \\ 94.58 \text{ kN} \\ -67.63 \text{ kNm} \end{bmatrix}$$

$$\hat{s}^2 = \begin{bmatrix} \hat{s}_1 \\ \hat{s}_2 \\ \hat{s}_3 \\ \hat{s}_4 \\ \hat{s}_5 \\ \hat{s}_6 \end{bmatrix} = \begin{bmatrix} 233800 & 0 & 0 & -233800 & 0 & 0 \\ 0 & 1997 & 2996 & 0 & -1997 & 2996 \\ 0 & 2996 & 5992 & 0 & -2996 & 2996 \\ -233800 & 0 & 0 & 233800 & 0 & 0 \\ 0 & -1997 & -2996 & 0 & 1997 & -2996 \\ 0 & 2996 & 2996 & 0 & -2996 & 5992 \end{bmatrix} \begin{bmatrix} 0.001488 \text{ m} \\ -0.007200 \text{ m} \\ -0.002370 \text{ rad} \\ 0 \text{ m} \\ 0 \text{ m} \\ 0 \text{ rad} \end{bmatrix} + \begin{bmatrix} 0 \\ 150 \\ 75 \\ 0 \\ 150 \\ -75 \end{bmatrix} = \begin{bmatrix} 347.89 \text{ kN} \\ 142.72 \text{ kN} \\ 67.63 \text{ kNm} \\ -347.89 \text{ kN} \\ 157.28 \text{ kN} \\ -89.47 \text{ kNm} \end{bmatrix}$$



Diyagramlar(klasik işaret kuralına göre):

